


EC ENGR101A-1

Mid-term (Total: 40 points)

Due: 2/9/21, 11:59 pm PST

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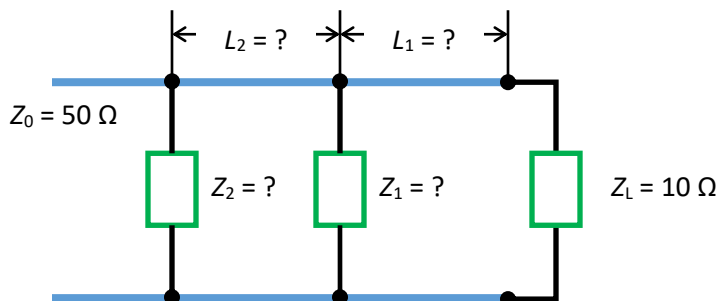
I,  , hereby, agree with the code of honor specified above.

Question #1 (8 points)

Please describe in your own words what key concepts have you learned for transmission lines.

Question #2 (8 points)

A $10\text{-}\Omega$ load can be matched to a $50\text{-}\Omega$ lossless transmission line by placing two shunt components $Z_1 (\neq \infty)$ and $Z_2 (\neq \infty)$ at distances $L_1 (\neq 0)$ and $L_1 + L_2 (L_2 \neq 0)$ respectively from the load. Determine their values using the Smith chart. (*Note: there are infinitely many solutions; any one of such solutions will do providing that you clearly indicate how your solution is obtained on the Smith chart.*)



Question #3 (8 points)

Given the vector field $\mathbf{A} = \hat{\phi} \sin(\phi/2)$, verify Stoke's theorem over the hemispherical surface and its circular contour that are shown in the following figure.

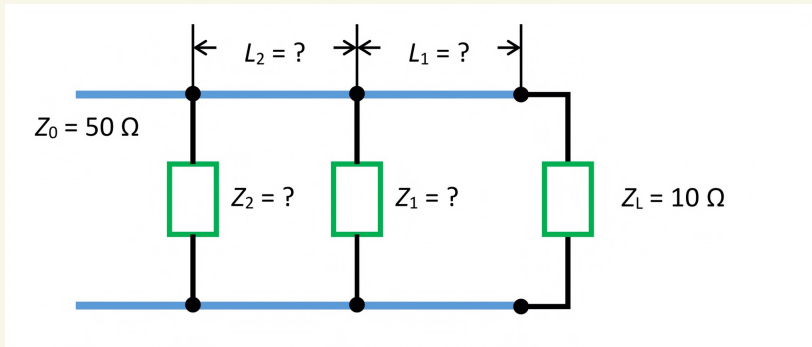
1) Please describe in your own words what key concepts have you learned for transmission lines.

A transmission line is something used in order to connect two different pieces of equipment, or in more general terms two points, and the transmission line is used to transfer energy or information between those two points.

Note: A transmission line will have two ports or terminals. One end of the transmission is connected to a source, which is the provider of energy, while the other is connected to the load, which takes in the energy. The transmission line transfers the energy. Some examples where we can see transmission lines used are power amplifiers, antenna rays, and filters. In a power amplifier we can see transmission lines used in order to guide the signal through the power amplifier. With a transmission line the information flowing through will travel in a sinusoidal wave shape. The wave can be modeled using a general expression that includes an attenuation constant, phase constant, angular frequency and a reference phase. An important factor to note is that for a pair of wires to be considered a transmission line, the wire line should be about 10 percent of the operating wavelength.

There are two main types of transmission lines, transverse electromagnetic (TEM) and higher order lines. The TEM moves in the x-y plane (where it propagates from) while the high order line has a component in all 3 xyz directions. When analyzing a transmission line we can use a lumped element model. Some parameters that can be seen in a transmission line are the resistance, inductance, conductance and capacitance. As we find these parameters, we need to adjust for to see if the transmission line is coaxial, two-wire, or a parallel plate. As we analyze the transmission line, we can use the wave equation for both voltage and current. These can be found with the help of Kirchhoff's voltage and current laws. As the wave travels in a sinusoidal time-domain we need to use phasors in order to accurately pinpoint the voltage and current of the wave. The voltage and current are related by a characteristic called the impedance. The impedance can have both real and imaginary parts but in lossless lines, the impedance is reduced to a real number. A lossless line is a line with no line resistance and no dielectric loss. The impedance can be found using a Smith chart and it allows for transmission lines to be manipulated. The Smith chart has both the impedance and admittance grids which also allow us to check values for circuits. In order to use a Smith chart we have to understand how to normalize the impedance and use a reflection coefficient, which is portrayed by Γ . We can rotate the Smith chart and it rotates in a clockwise fashion.

H 2)



Note: $Z_0 = 50 \Omega$
 $Z_L = 10 \Omega$

Normalized

$$\bar{Z}_L = \frac{Z_L}{Z_0} = \frac{10 \Omega}{50 \Omega} = 0.2$$

↑
on smith chart

$$\bar{Z}_{L,1} = 5.0 \quad \text{rotate } 0.25 \lambda$$

$$\downarrow$$

$$\bar{Z}_{L,1} = Z_0(\bar{Z}_{L,1})$$

$$\bar{Z}_{L,1} = (50 \Omega)(5.0)$$

$$= 250 \Omega$$

if we use $Z_1 = 375$

$$Z_{in,1} = \left(\frac{1}{Z_1} + \frac{1}{Z_{L,1}} \right)^{-1} = \left(\frac{1}{375} + \frac{1}{250} \right)^{-1} = 150$$

$$\bar{Z}_{in,1} = \frac{Z_{in,1}}{Z_0}$$

$$= \frac{150}{50} \Omega$$

$$= 3$$

↓
rotate by 0.5λ

$$\bar{Z}_{in,1} = \bar{Z}_{L,2} = 3.0$$

$$Z_{L,2} = (50 \Omega)(3) = 150 \Omega$$

↓

$$Z_{in,2} = Z_0 = 50 \Omega$$

$$z_{in,2} = \left(\frac{1}{z_2} + \frac{1}{z_{L2}} \right)^{-1}$$

$$\frac{1}{50} = \frac{1}{z_2} + \frac{1}{150}$$

$$\frac{1}{50} - \frac{1}{150} = \frac{1}{z_2}$$

$$\frac{3}{150} - \frac{1}{150} = \frac{1}{z_2}$$

$$z_2 = \frac{150}{2} = 75 \Omega$$

$$L_1 = 0.25 \lambda$$

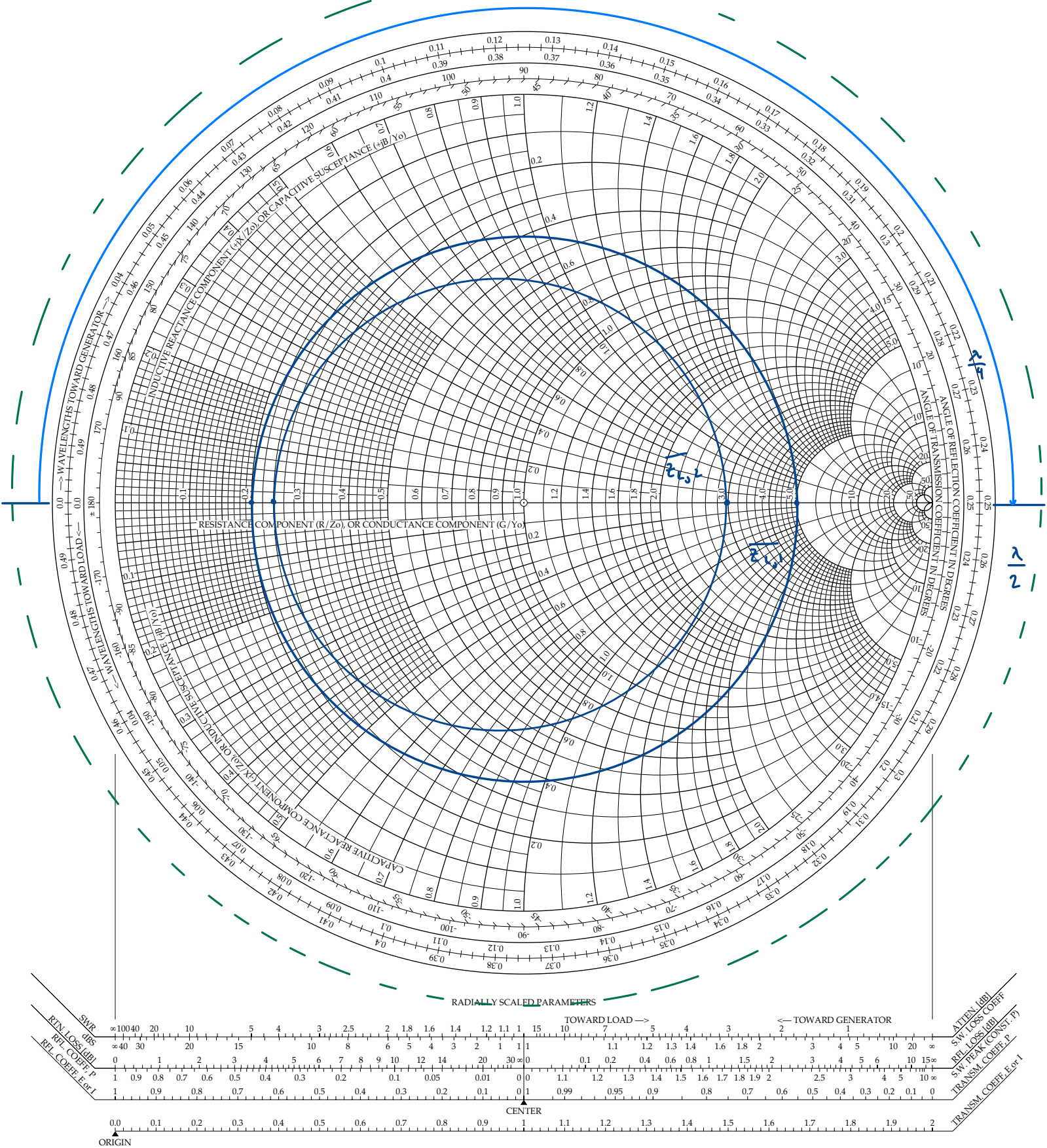
$$z_1 = 150 \Omega$$

$$L_2 = 0.5 \lambda$$

$$z_2 = 75 \Omega$$

The Complete Smith Chart

Black Magic Design

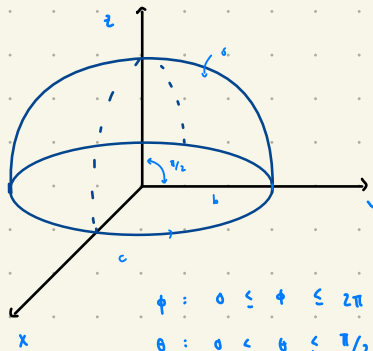


#3) $A = \hat{\phi} \sin(\phi/2)$ verify Stokes theorem

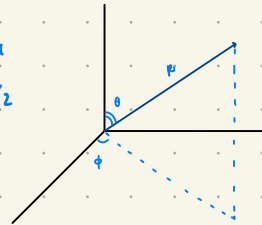
Stokes theorem

$$\int_V (\nabla \times \vec{B}) \cdot d\vec{v} = \oint_C \vec{B} \cdot d\vec{l}$$

WTS $A = \hat{\phi} \sin\left(\frac{\phi}{2}\right)$



$$\begin{aligned} \phi &: 0 \leq \phi \leq 2\pi \\ \theta &: 0 \leq \theta \leq \pi/2 \\ r &: b \end{aligned}$$



RHS

$$\oint_C \vec{B} \cdot d\vec{l}$$

$$\vec{B} = \hat{\phi} \sin\left(\frac{\phi}{2}\right)$$

$$d\vec{l} = \hat{r} dr + \hat{\theta} r d\theta + \hat{\phi} r \sin\theta d\phi$$

$$\vec{B} \cdot d\vec{l} = \left(\hat{\phi} \sin\left(\frac{\phi}{2}\right) \right) \cdot \left(\hat{r} dr + \hat{\theta} r d\theta + \hat{\phi} r \sin\theta d\phi \right)$$

$$= 0 + 0 + r \sin\theta \sin\left(\frac{\phi}{2}\right) d\phi$$

$$= r \sin\theta \sin\left(\frac{\phi}{2}\right) d\phi$$

$$\oint_C \vec{B} \cdot d\vec{l} = \int_{\phi=0}^{2\pi} r \sin\theta \sin\frac{\phi}{2} d\phi \Big|_{\theta=\pi/2} \Big|_{r=b}$$

$$= \int_{\phi=0}^{2\pi} b \sin(\pi/2) \sin\left(\frac{\phi}{2}\right) d\phi \Big|_{r=b}$$

$$= \int_{\phi=0}^{2\pi} b (1) \sin\left(\frac{\phi}{2}\right) d\phi \Big|_{r=b}$$

$$= \int_{\phi=0}^{2\pi} b \sin\left(\frac{\phi}{2}\right) d\phi$$

$$= b \int_{\phi} \sin\left(\frac{\phi}{2}\right) d\phi$$

$$= -b \cos\left(\frac{\phi}{2}\right) \left(\frac{1}{1/2}\right) \Big|_0^{2\pi}$$

$$= -2b \cos\left(\frac{\phi}{2}\right) \Big|_0^{2\pi}$$

$$= -2b \left(\cos\left(\frac{2\pi}{2}\right) - \cos(0) \right)$$

$$= -2b (-1 - 1)$$

$$= -2b(-2)$$

$$= 4b$$

$$\therefore \text{RHS} = 4b$$

LHS

$$\int_S (\nabla \times \vec{B}) \cdot d\vec{S}$$

$$\nabla \times \vec{B} = \frac{1}{r^2 \sin \theta} \begin{pmatrix} \hat{r} & \hat{\theta} & \hat{\phi} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ r & r \sin \theta & r \sin^2 \theta \end{pmatrix}$$

Note: $A = \hat{\phi} \sin\left(\frac{\phi}{2}\right)$

$$\begin{pmatrix} 0 & r(0) & r \sin \theta \sin\left(\frac{\phi}{2}\right) \\ r & r \cdot 0 & r \sin \theta \cdot \frac{1}{2} \end{pmatrix}$$

$$= \hat{r} \frac{1}{r \sin \theta} \left[\frac{\partial}{\partial \theta} A_{\phi} \sin \theta - \frac{\partial}{\partial \phi} A_{\theta} \right] + \hat{\theta} \frac{1}{r} \left[\frac{1}{\sin \theta} \frac{\partial}{\partial \phi} A_r - \frac{\partial}{\partial r} r A_{\phi} \right] + \hat{\phi} \frac{1}{r} \left[\frac{\partial}{\partial r} r A_{\theta} - \frac{\partial A_r}{\partial \theta} \right]$$

Note: $r = b$

$$= \hat{r} \frac{1}{b \sin \theta} \left(\frac{\partial}{\partial \theta} \sin\left(\frac{\phi}{2}\right) \sin \theta - \frac{\partial}{\partial \phi} 0 \right) + \hat{\theta} \frac{1}{b} \left[\frac{1}{\sin \theta} \frac{\partial}{\partial \phi} (2) - \frac{\partial}{\partial r} b \sin\left(\frac{\phi}{2}\right) \right] + \hat{\phi} \frac{1}{b} \left[\frac{\partial}{\partial r} b (0) - \frac{\partial}{\partial \theta} (0) \right]$$

$$= \hat{r} \frac{1}{b \sin \theta} \sin\left(\frac{\phi}{2}\right) \cos \theta + 0 + 0$$

$$= \hat{r} \frac{1}{b \sin \theta} \sin \frac{\phi}{2} \cos \theta$$

$$d\vec{S} = \hat{r} r^2 \sin \theta d\theta d\phi + \hat{\theta} r \sin \theta dr d\phi + \hat{\phi} r dr d\theta$$

↓

$$(\nabla \times \vec{B}) \cdot d\vec{S} = r^2 \sin \theta d\theta d\phi \cdot \frac{1}{b \sin \theta} \sin \frac{\phi}{2} \cos \theta$$

$$= \frac{r^2}{b} \sin \frac{\phi}{2} \cos \theta d\theta d\phi$$

Note: $r > b$

$$= \frac{b^2}{b} \sin \frac{\phi}{2} \cos \theta d\theta d\phi$$

$$= b \sin \frac{\phi}{2} \cos \theta d\theta d\phi$$

$$\int_S (\nabla \times \vec{B}) \cdot d\vec{S} = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi/2} b \sin \frac{\phi}{2} \cos \theta \, d\theta \, d\phi$$

$$= \int_{\phi=0}^{2\pi} b \sin \left(\frac{\phi}{2} \right) \left(\int_{\theta=0}^{\pi/2} \cos \theta \, d\theta \right) d\phi$$

Aside: $\int_{\theta=0}^{\pi/2} \cos \theta \, d\theta = \sin \theta \Big|_0^{\pi/2}$

$$= \sin \left(\frac{\pi}{2} \right) - \sin(0)$$

$$= (1 - 0)$$

$$= 1$$

$$= \int_{\phi=0}^{2\pi} b \sin \left(\frac{\phi}{2} \right) (1) \, d\phi$$

$$= b \int_{\phi=0}^{2\pi} \sin \frac{\phi}{2} \, d\phi$$

$$= b (-2) \cos \frac{\phi}{2} \Big|_{\phi=0}^{2\pi}$$

$$= -2b (\cos \pi - \cos 0)$$

$$= -2b (-1 - 1)$$

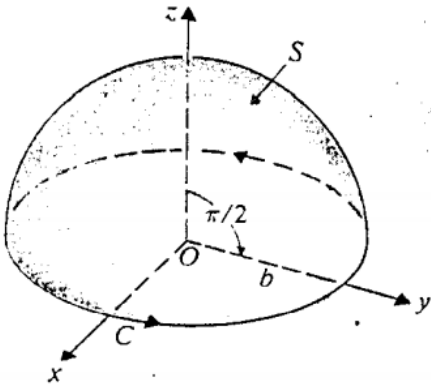
$$= -2b (-2)$$

$$= 4b$$

$$\therefore \text{LHS} = 4b$$

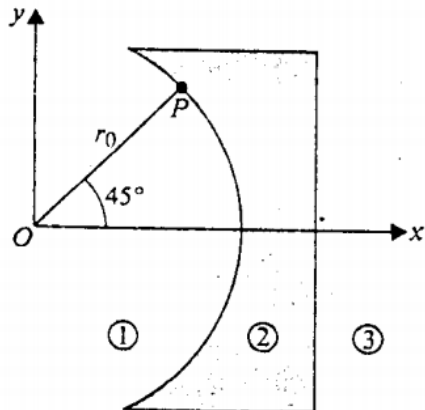
$$\text{Plc LHS} = \text{RHS}$$

$\hookrightarrow \therefore$ we have verified stoke's theorem



Question #4 (8 points)

Dielectric lenses can be used to collimate electromagnetic fields. In the following figure, the left surface of the lens is that of a circular cylinder, and the right surface is a plane. If \mathbf{E}_1 at point $P(r_0, 45^\circ, z)$ in region 1 is $\hat{\mathbf{r}}7 - \hat{\boldsymbol{\phi}}3$, what must be the dielectric constant of the lens in order that \mathbf{E}_3 in region 3 is parallel to the x-axis?

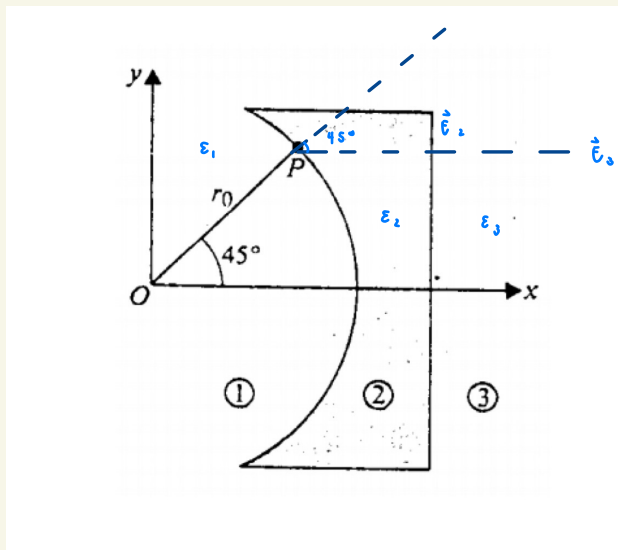


Question #5 (8 points)

Given a uniform sphere of charge (centered at origin) of radius R_0 and volume charge density ρ . In addition, the point at infinity acts as zero potential reference.

- Find the potential at a point outside the sphere ($R > R_0$).
- Find the potential at a point inside the sphere ($R \leq R_0$).
- Verify the solution obtained in part a) satisfies Laplace's equation.
- Verify the solution obtained in part b) satisfies Poisson's equation.

4)



$$P(r_0, 45^\circ, z) \quad \vec{E}_1 = \hat{r} 7 - \hat{\phi} 3$$

want $\vec{E}_3 \parallel x\text{-axis}$
 \hookrightarrow parallel

$$\begin{aligned} \vec{E}_1 &= \hat{r} E_{1r} + \hat{\phi} E_{1\phi} \\ \vec{E}_2 &= \hat{r} E_{2r} + \hat{\phi} E_{2\phi} \\ \vec{E}_3 &= \hat{r} E_{3r} + \hat{\phi} E_{3\phi} \end{aligned} \quad \rightarrow$$

$$\begin{aligned} \vec{E}_1 &= \hat{r} 7 - \hat{\phi} 3 \\ \hookrightarrow E_{1r} &= 7 \\ \hookrightarrow E_{1\phi} &= -3 \end{aligned}$$

Due to permittivity

$$\epsilon_3 = \epsilon_1 = \epsilon_0$$

$$\epsilon_2 = \epsilon_{\text{lens}} \cdot \epsilon_0$$

boundary and surface of dielectric lens

if $\vec{E}_3 \parallel x\text{-axis}$

$$\hookrightarrow \vec{E}_2 \parallel x\text{-axis}$$

$$\left. \begin{aligned} \vec{E}_3 \hat{y} &= 0 \\ \vec{E}_2 \hat{y} &= 0 \end{aligned} \right\} \text{bc parallel to } x\text{-axis}$$

\hookrightarrow in regions 2 and 3

converting

$$\hat{x} = \hat{r} \cos \phi - \hat{\phi} \sin \phi$$

$$\hat{y} = \hat{r} \sin \phi + \hat{\phi} \cos \phi$$

$$(\hat{r} E_{2r} + \hat{\phi} E_{2\phi}) \cdot (\hat{r} \sin \phi + \hat{\phi} \cos \phi) =$$

$$\downarrow$$
$$E_{2r} \sin \phi + E_{2\phi} \cos \phi = 0$$

point $P(r_0, 45^\circ, z)$

$$\phi = 45^\circ$$

$$\downarrow$$
$$E_{2r} \sin 45^\circ + E_{2\phi} \cos 45^\circ = 0$$

$$E_{2r} \frac{\sqrt{2}}{2} + E_{2\phi} \frac{\sqrt{2}}{2} = 0$$

$$\frac{\sqrt{2}}{2} (E_{2r} + E_{2\phi}) = 0$$

$$E_{2r} + E_{2\phi} = 0$$

$$E_{2r} = -E_{2\phi}$$

by observation of region 1 and 2

$$\rightarrow E_{1\phi} = E_{2\phi}$$

$$P(r_0, 45^\circ, z) \quad \vec{E}_1 = \hat{r} 7 - \hat{\phi} 3$$

$$\downarrow$$
$$E_{1\phi} = -3$$

$$E_{2\phi} = -3 \quad \text{or} \quad E_{2\phi} = -E_{2r}$$

$$E_{2r} = -(-3) = 3$$

electric flux density

$$\epsilon_1 E_1 \hat{r} = \epsilon_2 E_2 \hat{r}$$

$$E_1 E_{1r} = \epsilon_2 E_{2r} \quad \epsilon_2 = \epsilon_{\text{lens}} \cdot \epsilon_0$$

$$\epsilon_1 E_{1r} = \epsilon_{\text{lens}} \epsilon_0 E_{2r}$$

$$\epsilon_{\text{lens}} = \frac{E_{1r}}{E_{2r}} = \frac{7}{3}$$

$$\epsilon_{\text{lens}} = \frac{7}{3} \quad \text{or} \quad 2.33$$

uniform sphere of charge of radius R_0 and volume charge density ρ

5a) potential at point outside sphere $R > R_0$

$$\oint_S E_r ds = E_r \cdot 4\pi R^2 = \frac{Q_{\text{enclosed}}}{\epsilon_0}$$

$$Q_{\text{enclosed}} = \rho V_{\text{enclosed}}$$

$$Q_{\text{encl}} = \rho \frac{4}{3} \pi R_0^3$$

$$\oint_S E_r ds = E_r \cdot 4\pi R^2 = \frac{Q_{\text{enclosed}}}{\epsilon_0} = \frac{1}{\epsilon_0} \left(\rho \frac{4}{3} \pi R_0^3 \right)$$

$$\oint_S E_r ds = \frac{\rho 4\pi R_0^3}{3 \epsilon_0} = E_r \cdot 4\pi R^2$$

$$E_r = \frac{\rho 4\pi R_0^3}{3 \epsilon_0 4\pi R^2} \hat{r} = \frac{\rho R_0^3}{3 \epsilon_0 R^2} \hat{r}$$

$$V_R = - \int_{\infty}^R \frac{\rho R_0^3}{3 R^2 \epsilon_0} dR$$

$$= (-1) \frac{\rho R_0^3}{3 \epsilon_0} \int_{\infty}^R \frac{1}{R^2} dR$$

$$\left(\text{ASIDE: } \int_{\infty}^R \frac{1}{R^2} = \frac{R^{-1}}{-1} \Big|_{\infty}^R = (-1) \left(\frac{1}{R} - \frac{1}{\infty} \right) = -\frac{1}{R} \right)$$

$$= (-1) \frac{\rho R_0^3}{3 \epsilon_0} \frac{(-1)}{R}$$

$$V_R = \frac{\rho R_0^3}{3 \epsilon_0 R} \quad (R > R_0)$$

5b) potential a point inside the sphere ($r \leq R_0$)

$$\oint_S \epsilon_r ds = \epsilon_r \cdot 4\pi r^2 = \frac{Q_{\text{enclosed}}}{\epsilon_0}$$

$$Q_{\text{encl}} = \rho V_{\text{encl}} = \rho \frac{4}{3} \pi r^3$$

$$\frac{Q_{\text{encl}}}{\epsilon_0} = \frac{\rho 4\pi r^3}{3\epsilon_0} = \oint \epsilon_r ds$$

$$\epsilon_r 4\pi r^2 = \oint \epsilon_r ds$$

$$\Downarrow$$
$$\epsilon_r 4\pi r^2 = \frac{\rho 4\pi r^3}{3\epsilon_0}$$

$$\epsilon_r = \frac{\rho 4\pi r^3}{3\epsilon_0} \frac{1}{4\pi r^2}$$
$$= \frac{\rho r}{3\epsilon_0}$$

$$V_r = - \int \epsilon_r dr = - \int \frac{\rho r}{3\epsilon_0} dr$$

$$= - \frac{\rho}{3\epsilon_0} \int r dr$$

$$= - \frac{\rho}{3\epsilon_0} \frac{r^2}{2}$$

$$V_r = - \frac{\rho r^2}{6\epsilon_0} \quad ; \quad r \leq R_0$$

so) verify part a satisfies Laplace's Eqn

Laplace Eqn

$$\nabla^2 V = 0$$

$$V = \frac{\rho R_0^3}{3 \epsilon_0 R} = \frac{\rho R_0^3}{3 \epsilon_0} R^{-1}$$

$$\frac{d}{dR} V = \frac{\rho R_0^3}{3 \epsilon_0} (-1) R^{-2} \longrightarrow \frac{(-1) \rho R_0^3}{3 \epsilon_0 R^2}$$

$$\frac{d^2}{dR^2} V = \frac{\rho R_0^3}{3 \epsilon_0} (-1)(-2) R^{-3} \longrightarrow \frac{2 \rho R_0^3}{3 \epsilon_0 R^3}$$

$$\nabla \cdot \nabla V = \frac{d^2}{dR^2} V + \frac{2}{R} \frac{d}{dR} V$$

$$= \frac{2 \rho R_0^3}{3 \epsilon_0 R^3} + \frac{2}{R} \cdot \frac{(-1) \rho R_0^3}{3 \epsilon_0 R^2}$$

$$= \frac{2 \rho R_0^3}{3 \epsilon_0 R^3} - \frac{2 \rho R_0^3}{3 \epsilon_0 R^3}$$

$$= 0$$

$$\therefore \nabla^2 V = 0$$

Laplace eqn is satisfied

5d) verify part b satisfy's poisson equation

Poisson Eqn

$$\nabla^2 V = \frac{-\rho V}{\epsilon} = \frac{-\rho}{\epsilon_0}$$

$$V = \frac{-\rho R^2}{6\epsilon_0} \quad \text{from part b}$$

$$\frac{\partial}{\partial R} V = \frac{-\rho}{6\epsilon_0} 2R \rightarrow \frac{-\rho R}{3\epsilon_0}$$

$$\frac{\partial^2}{\partial R^2} V = \frac{-\rho}{3\epsilon_0}$$

$$\nabla(\nabla V) = \frac{\partial^2}{\partial R} V + \frac{2}{R} \frac{\partial V}{\partial R}$$

$$= \frac{-\rho}{3\epsilon_0} + \frac{2}{R} \frac{-\rho R}{3\epsilon_0}$$

$$= \frac{-\rho}{3\epsilon_0} - \frac{2\rho}{3\epsilon_0}$$

$$= (-1) \frac{(1+2)}{3} \frac{\rho}{\epsilon_0}$$

$$\therefore \nabla^2 V = \frac{-\rho}{\epsilon_0} \quad \text{Poisson's Eqn is satisfied}$$