

# SOLUTIONS

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UCLA Department of Electrical Engineering  
EE101 – Engineering Electromagnetics  
Winter 2011  
Midterm, February 7 2011, (1:45 minutes)

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Name \_\_\_\_\_ Student number \_\_\_\_\_

This is a closed book exam – you are allowed 1 page of notes (front+back).

Check to make sure your test booklet has all of its pages – both when you receive it and when you turn it in.

Remember – there are several questions, with varying levels of difficulty, be careful not to spend too much time on any one question to the exclusion of all others.

Exam grading: When grading, we focusing on evaluating your level of understanding, based on what you have written out for each problem. For that reason, you should make your work clear, and provide any necessary explanation. In many cases, a correct numerical answer with no explanation will not receive full credit, and a clearly explained solution with an incorrect numerical answer will receive close to full credit. CIRCLE YOUR FINAL ANSWER.

If an answer to a question depends on a result from a previous section that you are unsure of, be sure to write out as much of the solution as you can using symbols before plugging in any numbers, that way at you will still receive the majority of credit for the problem, even if your previous answer was numerically incorrect.

Please be neat – we cannot grade what we cannot decipher.

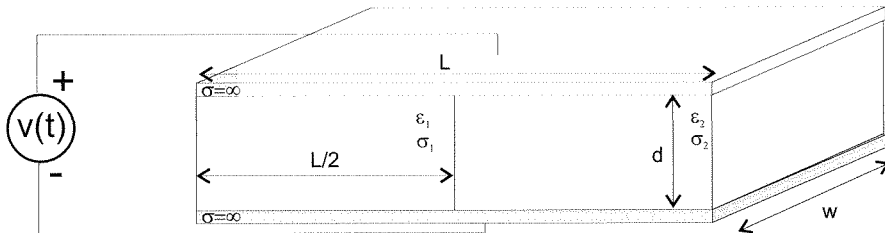
	Topic	Max Points	Your points
Problem 1	Capacitor	35	
Problem 2	Kirchoff's Laws	30	
Problem 3	Solenoid	35	
Total		100	

Note: Because of photo copying error, Problems 1(b) + 2(b) are missing.  
Every one received effective full credit for the missing questions.  
1(b) → 5pts  
2(b) → 15pts

1. Capacitor

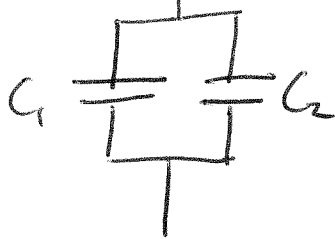
<sup>35</sup>  
~~40~~ points)

In this problem, we consider a parallel plate capacitor shown below where two metal (assume perfectly conducting) plates are separated by distance  $d$ . Assume that the lateral dimensions  $L, b \gg d$  so that we can make a 1D approximation and neglect fringing fields. The capacitor is filled with two types of dielectric materials, with permittivity  $\epsilon_1$ , and  $\epsilon_2$  assume  $\epsilon_2 > \epsilon_1$ . Because the dielectric material isn't perfect, the material has some small conductivity  $\sigma_1$ , and  $\sigma_2$  respectively.



- (a) <sup>15</sup>  
~~10~~ points) If you neglect the conductivity, what is the capacitance of this capacitor, in terms of the dimensions and material properties?

Equivalent to two capacitors in parallel.



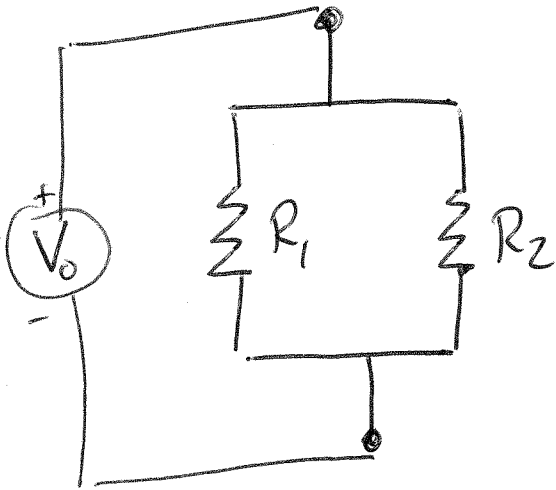
$$C_1 = \frac{WL\epsilon_1}{2d}$$

$$C_2 = \frac{WL\epsilon_2}{2d}$$

$$C_{total} = C_1 + C_2 = \frac{LW}{2d} (\epsilon_1 + \epsilon_2)$$

- (c) (15 points) Now consider the leakage conductance of the dielectric – give an expression for the resistance  $R$  of this capacitor in terms of the material properties and the dimensions.

Consider two resistors in parallel.

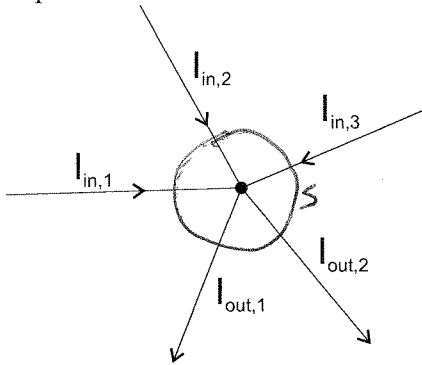


$$R_1 = \frac{2d}{\sigma_1 LW} \quad R_2 = \frac{2d}{\sigma_2 LW}$$

$$R = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2}} = \frac{2d}{LW} \frac{1}{\sigma_1 + \sigma_2}$$

## 2. Kirchoff's Laws (30 points)

- (15 pts) (a) In circuit theory, Kirchoff's current law says that the sum of the currents flowing into a circuit node is equal to the sum of the currents flowing out:  $\sum_n I_{in,n} = \sum_m I_{out,m}$ . Give a physical explanation/derivation for this rule, citing equations as needed.



Ampere's Law

$$\nabla \cdot (\nabla \times \mathbf{H}) = \nabla \cdot \mathbf{J} + \nabla \cdot \frac{\partial \mathbf{D}}{\partial t}$$

$$\boxed{\nabla \cdot \mathbf{J} = -\frac{\partial \rho}{\partial t}} \quad \text{Current continuity}$$

Apply the current continuity equation  $\nabla \cdot \mathbf{J} = -\frac{\partial \rho}{\partial t}$  in integral form with a surface around the node:

$$\oint \vec{\mathbf{J}} \cdot d\vec{\mathbf{S}} = -\frac{d}{dt} Q_{enc}$$

In steady state  $\frac{dQ}{dt} = 0$  since charge cannot build up in a circuit node in dc (otherwise Coulomb repulsion will create a field to keep current flowing).

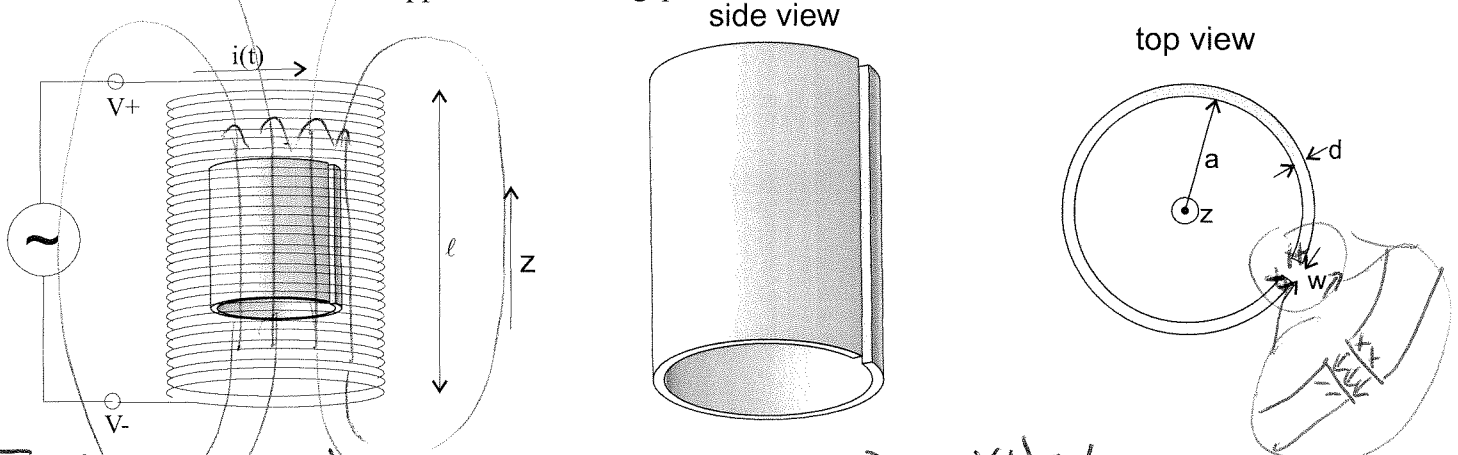
Therefore  $\oint \vec{\mathbf{J}} \cdot d\vec{\mathbf{S}} = 0$  in steady state,

which means total current in = total current out at any point in a circuit.

3. Solenoid (30 points)

- a. (15 points) Consider a cylindrical metal shell with conductivity  $\sigma$  placed inside a long solenoid of length  $l$  with  $N$  turns driven to produce a magnetic field. The shell has a small gap in the edge as shown (width  $w \ll a$ ). The current in the solenoid is  $i(t) = kt$ , where  $k$  is a positive constant (units of A/s), with a direction as indicated in the figure. The shell has dimensions as shown, where  $d \ll a$ .

What is the current density  $\mathbf{J}(\phi, t)$  flowing in the metal shell? What is the potential difference that appears across the gap?



Field generated by solenoid inside:  $\vec{H} = \frac{i(t)N}{l} \hat{z} = \frac{ktN}{l} \hat{z}$

$\frac{d\vec{H}}{dt} = z \frac{kN}{l}$  (this creates a steady emf)

This will induce an emf around circumference of metal shell.

$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \Rightarrow \oint \vec{E} \cdot d\vec{l} = -\frac{d}{dt} \int \vec{B} \cdot d\vec{S} = -\frac{d}{dt} \Phi$

Choose loop through circumference of metal.

$\frac{d}{dt} \Phi = -\pi a^2 \mu_0 \frac{kN}{l} = \oint \vec{E} \cdot d\vec{l} = E_\phi 2\pi a$

$E_\phi = \frac{-\mu_0 kN a}{l 2}$

See next page for alternate sol'n.

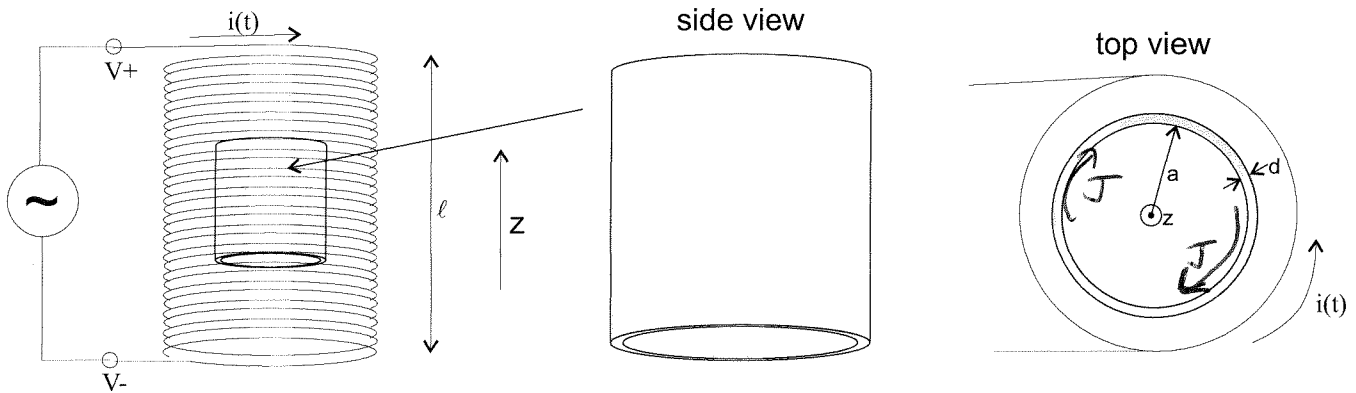
$\mathbf{J} = 0$  because gap won't let current flow in steady state.  
 Potential across gap =  $\int d\phi = E_\phi = 2\pi a E_\phi = \frac{-\pi a^2 \mu_0 kN}{l}$

- b. (15 points) Now consider if the metal shell has no gap as shown. Once again,  $i(t)=kt$ . What is the current density  $\mathbf{J}(\phi,t)$  flowing in the metal shell, and which direction does it flow? Your answer should be as a function of dimensional parameters,  $k$ , etc. -  $H$  should not appear in your final answer.

You may wish to refer to the relationship we derived in class for a metal shell in a z-oriented H-field:

$$\frac{\partial}{\partial t} H_m + \frac{H_m}{\tau_m} = \frac{H_0}{\tau_m}, \quad \text{where } \tau_m = d\sigma a\mu_0/2 \text{ is the magnetic diffusion time, and where}$$

$H_1(t)$  is the field generated by currents in the metal shell,  $H_0(t)$  is the externally applied  $H$  field in the z-direction resulting from the solenoid, and  $H_{in}(t)=H_1(t)+H_0(t)$  is the total axial H-field inside the metal shell (all H-fields are defined to be oriented in the z-direction).



The steady increase in  $i(t)$  creates a steady increase in  $H_0(t) = \frac{k t N}{l}$

$\frac{dH_0}{dt} = \frac{kN}{l} \Rightarrow$  This will create a steady emf which drives a steady current density

$$\mathbf{J}_\phi = \sigma E_\phi = -\frac{\mu_0 k N a}{l} \frac{1}{2} \sigma \hat{\phi}$$

While this  $\mathbf{J}$  will create its own magnetic field  $H_1$ ,

since  $\mathbf{J}_\phi$  is steady ( $\frac{d\mathbf{J}}{dt} = 0$ ),  $\frac{dH_1}{dt} = 0$ , + only

$\frac{dH_0}{dt} = \frac{dH_{in}}{dt}$  will contribute to the emf in the shell.

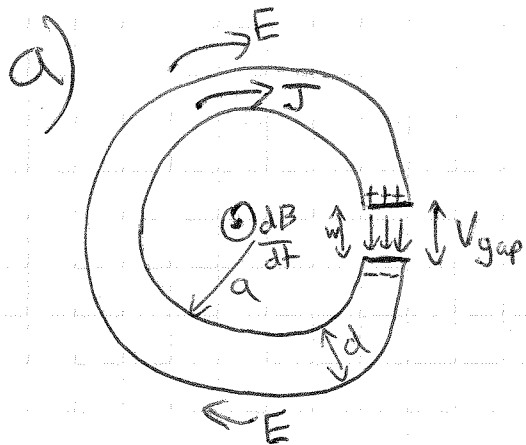
See next page for transient response

# Problem 3 Addendum - Transient Case (not required)

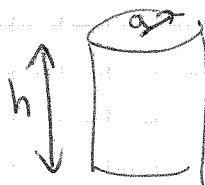
While the problem specified a steadily increasing solenoid current  $i(t) = kt$ , some of you interpreted this as

$$i(t) = \begin{cases} 0 & t < 0 \\ kt & t > 0 \end{cases}$$

This will cause a turn-on transient in the response.

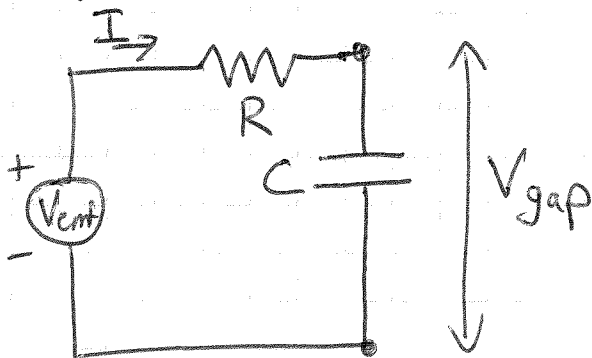


After an initial turn on of current, the gap will act as a capacitor, to produce an opposite field that counteracts the emf field, & stops the current from flowing.



$h$  = height of metal cylinder

Equivalent Circuit



$R$  is resistance of conductor

(assume  $w \ll a$ )

$$R = \frac{2\pi a}{\sigma d h}$$

$$C \approx \frac{\epsilon_0 h d}{w}$$

(assume  $w \ll d$   
parallel plate capacitor approx)

$$RC = \frac{2\pi a}{w} \frac{\epsilon_0}{\sigma}$$

Dielectric relaxation time for this circuit

When  $i(t)$  is turned on at  $t=0$

$$V_{emf} = -\frac{d\Phi}{dt}$$

$$2\pi a E_p = -\frac{\pi a^2 \mu_0 k N}{l}$$

a) continued

$$\frac{I}{R} = \frac{V_{emf} - V_{gap}}{R} = \frac{C dV_{gap}}{dt} \Rightarrow$$

Inhomogeneous ODE

$$V_{emf} = V_{gap} + RC \frac{dV_{gap}}{dt}$$

Sol'n to ODE:

$$V_{gap} = V_{emf} (1 - e^{-t/RC})$$

Initial cond:  
 $V_{gap}(t=0) = 0$

Final cond:  
 $V_{gap}(t \rightarrow \infty) = V_{emf}$

$$V_{gap} = \frac{\pi a^2 \mu_0 k N}{l} (1 - e^{-t/RC})$$

as  $t \rightarrow \infty$   $V_{gap}$  reaches steady constant value:  $\frac{\pi a^2 \mu_0 k N}{l}$

$$J = \frac{I}{dh} = -\hat{\phi} \frac{\sigma a \mu_0 k N}{2l} e^{-t/RC}$$

as  $t \rightarrow \infty$ ,  $J \rightarrow 0$ , which makes sense.

Steady current can't flow across a gap.

The process takes several RC times to settle down.

For a good conductor like Copper  $\frac{\epsilon_0}{\sigma} \sim 10^{-19} \text{ s}$

Very fast!

Current only flows for a short time!



b) No gap  $i(t) = \begin{cases} 0 & t < 0 \\ kt & t > 0 \end{cases}$

Now we can use the differential eq we derived in class for a metal pipe in an axial magnetic field.

$$\frac{\partial}{\partial t} H_m + \frac{H_m}{\tau_m} = \frac{H_0}{\tau_m}$$

$$H_0 = kN/l$$

$$H_m = H_0 + H_i$$

$$H_i = J_s = J d \quad (\text{in metal shell})$$

$$\tau_m = \frac{\sigma \mu_0 d a}{2}$$

$$\frac{\partial}{\partial t} H_0 + \frac{\partial}{\partial t} H_i + \frac{H_i}{\tau_m} + \frac{H_0}{\tau_m} = \frac{H_0}{\tau_m}$$

$$\boxed{\frac{d}{dt} H_i + \frac{H_i}{\tau_m} = -\frac{d}{dt} H_0}$$

Solve inhomogeneous ODE

Homogeneous sol'n:  $H_{i,h} = A e^{-t/\tau_m}$

Particular sol'n:  $H_{i,p} = B \frac{d}{dt} H_0 = B \frac{kN}{l}$

Full sol'n:  $H_i(t) = A e^{-t/\tau_m} + B \frac{kN}{l}$   $A, B = \text{coeff}$

Init cond  $H_i(t=0) = 0$  Final cond  $t \rightarrow \infty$  steady state

$$B = -\tau_m \quad A = \tau_m kN/l \quad H_i(t \rightarrow \infty) = -\frac{\tau_m kN}{l}$$

$$H_i(t) = -\frac{\tau_m kN}{l} (1 - e^{-t/\tau_m})$$

$$H_m = H_0 + H_i = \frac{\tau_m kN}{l} \left( \frac{t}{\tau_m} - 1 + e^{-t/\tau_m} \right)$$

$$\boxed{\vec{J}(t) = -\hat{\phi} \frac{\tau_m kN}{d l} (1 - e^{-t/\tau_m}) = -\hat{\phi} \frac{\sigma \mu_0 kN}{2l} (1 - e^{-t/\tau_m})}$$

After several  $\tau_m$  ( $t \rightarrow \infty$ )  $J$  goes to a steady value  

$$\vec{J} = -\hat{\phi} \frac{\tau_m kN}{d l} = -\hat{\phi} \frac{\sigma \mu_0 kN}{2l}$$