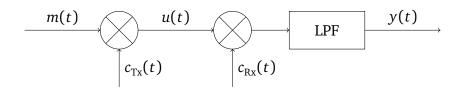
## **Midterm Exam - Solutions**

1. A DSB-SC modulated signal, u(t), is demodulated by applying it to a *coherent detector*. Assume the carrier used at the transmitter is given by  $c_{Tx}(t) = A_c \cos(2\pi f_c t)$ , while the carrier used by the receiver has a frequency error  $\Delta f$ , i.e.,  $c_{Rx} = \cos(2\pi (f_c + \Delta f)t)$ .



The cutoff frequency of the LPF is W Hz.

(a) (5 points) Evaluate the effect of the frequency error,  $\Delta f$ , in the demodulator's local carrier, i.e., write the expression of y(t), the output of the low-pass filter, assuming that  $\Delta f \ll f_c$  and  $\Delta f \ll W$ , where W is the bandwidth of the message signal, m(t).

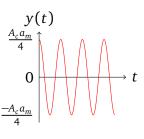
**Solution:** The received signal is  $r(t) = u(t) = A_c m(t) \cos(2\pi f_c t)$ . Thus,  $r(t) \cos(2\pi (f_c + \Delta f)t) = A_c m(t)m(t) \cos(2\pi f_c t) \cos(2\pi (f_c + \Delta f)t)$   $= \frac{A_c m(t)}{2} (\cos(2\pi \Delta f t) + \cos(2\pi (2f_c + \Delta f)t)).$ The output signal is  $y(t) = \frac{A_c m(t)}{2} \cos(2\pi \Delta f t) \star 2W \operatorname{sinc}(2W t)$ , where  $\mathcal{F}^{-1}[\Pi(\frac{f}{2W})] = 2W \operatorname{sinc}(2W t)$ .

(b) (5 points) Write the expression of Y(f) in terms of M(f).

**Solution:** 
$$Y(f) = \frac{A_c}{4} \left( M(f - \Delta f) + M(f + \Delta f) \right) \prod(\frac{f}{2W}), \text{ for } |f| \le W.$$

(c) (5 points) Assume  $m(t) = a_m \cos(2\pi f_m t)$ . Illustrate your answer by writing the expression of y(t) and sketching the demodulated signal. (Note that  $f_m = W$ .)

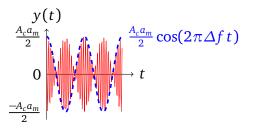
**Solution:** After the lowpass filter with bandwidth  $W = f_m$  (not including  $f_m + \Delta f$ ),  $y(t) = \frac{A_c a_m}{4} \cos(2\pi (f_m - \Delta f)t)$  Drawing of y(t) is given as:



**Solution:** After the lowpass filter with bandwidth  $W = f_m$  (including  $f_m + \Delta f$ ),

$$y(t) = \frac{A_c a_m}{2} \cos(2\pi f_m t) \cos(2\pi \Delta f t).$$

Drawing of y(t) is given as:



(d) (5 points) Still assuming  $m(t) = a_m \cos(2\pi f_m t)$ , plot the amplitude spectrum of y(t).

**Solution:**  $M(f) = \frac{a_m}{2} (\delta(f - f_m) + \delta(f + f_m))$ . When the frequency components of  $f_m + \Delta f$  and  $-f_m - \Delta f$  are not included, we obtain

$$Y(f) = \frac{A_c a_m}{8} \left( \delta(f - \Delta f + f_m) + \delta(f + \Delta f - f_m) \right).$$

$$(f) = \frac{A_c a_m}{8} \left( \delta(f - \Delta f + f_m) + \delta(f + \Delta f - f_m) \right).$$

**Solution:**  $M(f) = \frac{a_m}{2} (\delta(f - f_m) + \delta(f + f_m))$ . When the frequency components of  $f_m + \Delta f$  and  $-f_m - \Delta f$  are included, we obtain

$$Y(f) = \frac{A_c a_m}{8} \left( \delta(f - \Delta f + f_m) + \delta(f + \Delta f - f_m) + \delta(f + \Delta f + f_m) + \delta(-f - \Delta f - f_m) \right).$$

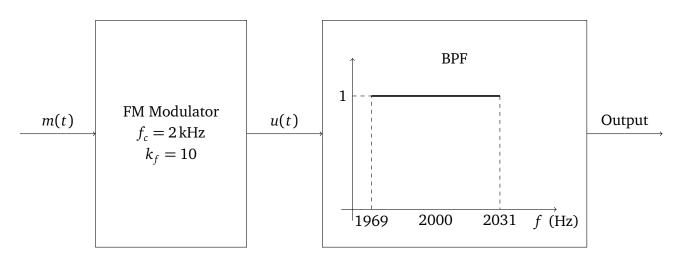
## 2. (20 points) The modulating signal that is input to an FM modulator is given by

 $m(t) = 10\cos(16\pi t), \text{ for } t \ge 0.$ 

The output of the FM modulator is

$$u(t) = 10\cos\left(4000\pi t + 2\pi k_f \int_{-\infty}^t m(\tau) d\tau\right),$$

where  $k_f = 10$ , see figure below.



If the output of the modulator, u(t) is passed through an ideal BPF centered at  $f_c$  and with a bandwidth of 62 Hz, determine the power of the frequency components at the output of the filter. Please compute the percentage of the power of u(t) that appears at the output of the BPF?

**Solution:**  $\int_{-\infty}^{t} m(\tau) d\tau = \frac{10}{16\pi} \sin(16\pi t)$ . We denote  $\beta = 2\pi k_f \frac{10}{16\pi} = 10 \frac{10}{8} = 12.5$ ,  $f_c = 2000$  [Hz],  $A_c = 10$  [V] and  $f_m = 8$  [Hz]. Thus,  $u(t) = A_c \cos(2\pi f_c t + \beta \sin(2\pi f_m t))$ . Then, u(t) can be expressed as:

$$u(t) = \sum_{n=-\infty}^{\infty} A_c J_n(\beta) \cos(2\pi (f_c + nf_m)t).$$

The power of the frequency components at the output of the filter is

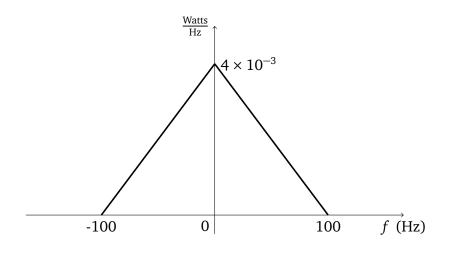
$$\frac{A_c^2}{2} \sum_{n=-3}^{3} J_n^2(\beta) = 8.35 \text{ [Watts],}$$

or 3.5 [Watts] (if only use fist decimal digit). The total power of u(t) is  $\frac{A_c^2}{2} = 50$  [Watts]. As a result, the percentage of the power of u(t) that appears at the output of the BPF is given as:

$$\sum_{n=-3}^{3} J_n(\beta)^2 = J_0(\beta)^2 + 2 \times \sum_{n=1}^{3} J_n(\beta)^2 = 0.1607 = 16.7\%,$$

or 7% (if only use first decimal digit and truncate the second decimal digit).

3. A message signal, m(t), such that  $-2 \le m(t) \le 2$  volts has power spectral density given by



The white Gaussian noise on the channel has a power spectral density  $\frac{N_0}{2}$ , where  $N_0 = 1 \times 10^{-6} \frac{\text{W}}{\text{Hz}}$ .

(a) (5 points) Assuming that the message modulates a carrier of amplitude  $A_c = 1$  V in a DSB-SC scheme, what is the signal-to-noise ratio at the output of the coherent demodulator? (Assume that the receiver is perfectly synchronized to the transmitter.)

**Solution:** The output  $y(t) = \frac{1}{2}A_c m(t) + \frac{n_c(t)}{2}$ . The signal power is  $P_{o,s} = \frac{A_c^2}{4}P_M = 0.25 \times 0.4 = 0.1$  [watts]. The noise power is  $P_{o,n} = \frac{1}{4}2N_0W = 0.25 \times 2 \times 10^{-6} \times 100 = 5 \times 10^{-5}$  [watts]. Thus, the corresponding SNR is  $\frac{0.1}{5 \times 10^{-5}} = 2000$ .

(b) (5 points) If m(t) modulates the same carrier in a conventional AM scheme with a modulation index = 0.9, what is the signal-to-noise ratio at the output of the envelope detector, after the DC has been removed? (Can you make the assumption that the received signal-to-noise ratio is high?)

**Solution:** After removing the DC component, we obtain the output of the envelope detector is  $y(t) = A_c a m_n(t) + n_c(t)$ . Since  $|m(t)| \le 2$ , then  $m_n(t) = \frac{m(t)}{2}$ . The power content of  $m_n(t)$  is  $P_{m_n} = \frac{P_m}{4} = 0.1$  [Watts]. The signal power is  $P_{o,s} = A_c^2 a^2 P_{M_n}$  [Watts]. The noise power is  $P_{o,n} = 2WN_0$  [watts]. Since modulation index is a = 0.9, the corresponding SNR =  $\frac{A_c^2 a^2 P_{M_n}}{2WN_0} = \frac{0.9^2 \times \frac{P_M}{4}}{2 \times 10^{-4}} = 405$ . Thus, we can assume that the received signal-to-noise ratio is high.

(c) (5 points) Still assuming a conventional AM scheme with a modulation index = 0.90, what is the signal-to-noise ratio at the output of the coherent detector, after the DC has been removed?

**Solution:** 
$$y(t) = \frac{A_c a m_n(t)}{2} + \frac{n_c(t)}{2}$$
. The output  $\text{SNR} = \frac{\frac{1}{4} A_c^2 a^2 P_{M_n}}{\frac{1}{4} 2 W N_0} = \frac{0.9^2 \times 0.1}{2 \times 10^{-4}} = 405$ .

(d) (5 points) Which of the two modulation schemes, DSB-SC or conventional AM, guarantees a higher signal-to-noise ratio at the output of the corresponding demodulator?

**Solution:** We observe that DSB-SC AM can guarantee a higher signal-to-noise ratio at the output of the corresponding demodulator.