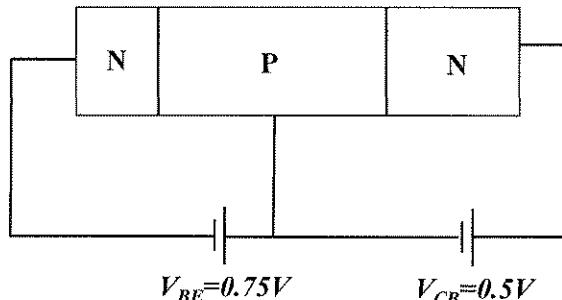
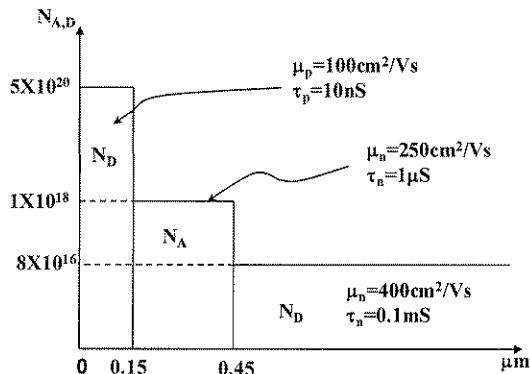


**EE 121B Mid-term Examination
Spring 2010**

Name _____

**Open Book
Assume T=300K and the substrate is silicon**

1) Consider the following bipolar transistor



$$A = 100 \mu\text{m}^2$$

- a) What is the neutral base width of the device with the DC biases as indicated? (5 points)

$$N_{DE} = 5 \times 10^{20} / \text{cm}^3, \quad N_{AB} = 1 \times 10^{18} / \text{cm}^3, \quad N_{DC} = 8 \times 10^{16} / \text{cm}^3, \quad V_{BE} = 0.75 \text{V}, \quad V_{CB} = 0.5 \text{V}$$

$$V_{bi-BE} = \frac{kT}{q} \ln \frac{N_{DE} N_{AB}}{n_i^2} = 0.026 \times \ln \frac{5 \times 10^{20} \times 1 \times 10^{18}}{1 \times 10^{20}} \approx 1.12 \text{V}$$

$$V_{bi-BC} = \frac{kT}{q} \ln \frac{N_{DC} N_{AB}}{n_i^2} = 0.026 \times \ln \frac{8 \times 10^{16} \times 1 \times 10^{18}}{1 \times 10^{20}} \approx 0.89 \text{V}$$

$$X_{p1} = \sqrt{\frac{2\varepsilon}{q} \frac{N_{DE}}{N_{AB}(N_{DE} + N_{AB})} \cdot (V_{bi-BE} - V_{BE})}$$

$$= \sqrt{\frac{2 \times 11.7 \times 8.85 \times 10^{-14}}{1.6 \times 10^{-19}} \cdot \frac{5 \times 10^{20}}{1 \times 10^{18} (5 \times 10^{20} + 1 \times 10^{18})} \cdot (1.12 - 0.75)} \approx 2.19 \times 10^{-6} \text{cm} = 21.9 \text{nm}$$

$$X_{p2} = \sqrt{\frac{2\varepsilon}{q} \frac{N_{DC}}{N_{AB}(N_{DC} + N_{AB})} \cdot (V_{bi-BC} + V_{CB})}$$

$$= \sqrt{\frac{2 \times 11.7 \times 8.85 \times 10^{-14}}{1.6 \times 10^{-19}} \cdot \frac{8 \times 10^{16}}{1 \times 10^{18} (8 \times 10^{16} + 1 \times 10^{18})} \cdot (0.89 + 0.5)} \approx 1.15 \times 10^{-6} \text{cm} = 11.5 \text{nm}$$

$$W_{BM} = 0.45 - 0.15 = 0.3 \mu\text{m}$$

$$\therefore W_B = W_{BM} - X_{p1} - X_{p2}$$

$$= 0.3 \mu\text{m} - 21.9 \text{nm} - 11.5 \text{nm}$$

$$= 266.6 \text{nm}$$

b) What is the values of I_C , I_E , and I_B ? (15 points)

$$I_E \approx \frac{qAD_{nB}}{W_B} \cdot \frac{n_i^2}{N_{AB}} \cdot (e^{qV_{BE}/kT} - 1) + \frac{qAD_{pE}}{W_E} \cdot \frac{n_i^2}{N_{pE}} \cdot (e^{qV_{BE}/kT} - 1)$$

$$X_{n1} = \frac{X_{p1} \cdot N_{AB}}{N_{pE}} = \frac{21.9 \times 1 \times 10^{18}}{5 \times 10^{20}} \approx 0.0438 \text{ nm}$$

$$W_E = W_{EM} - X_{n1} = 0.15 \mu\text{m} - 0.0438 \text{ nm} \approx 150 \text{ nm}$$

$$J_{nB} = 250 \text{ cm}^2/\text{Vs} \Rightarrow D_{nB} = \frac{kT}{q} \cdot \mu_{nB} = 0.026 \times 250 = 6.5 \text{ cm}^2/\text{s}.$$

$$\mu_{pE} = 100 \text{ cm}^2/\text{Vs} \Rightarrow D_{pE} = \frac{kT}{q} \cdot \mu_{pE} = 0.026 \times 100 = 2.6 \text{ cm}^2/\text{s}.$$

$$\therefore I_E = \frac{1.6 \times 10^{-19} C \times 100 \times 10^{-8} \text{ cm}^2 \times 6.5 \text{ cm}^2/\text{s}}{266.6 \times 10^{-7} \text{ cm}} \cdot \frac{1 \times 10^{20} / \text{cm}^3}{1 \times 10^{18} / \text{cm}^3} \cdot e^{0.75 / 0.026}$$

$$+ \frac{1.6 \times 10^{-19} \times 100 \times 10^{-8} \times 2.6}{150 \times 10^{-7}} \cdot \frac{1 \times 10^{20}}{5 \times 10^{20}} \cdot e^{0.75 / 0.026}$$

$$\approx 1.31 \times 10^{-5} \text{ A} + 1.87 \times 10^{-8} \text{ A}$$

$$\approx 1.312 \times 10^{-5} \text{ A}$$

$$I_C \approx \frac{qAD_{nB}}{W_B} \cdot \frac{n_i^2}{N_{AB}} \cdot (e^{qV_{BE}/kT} - 1) \approx 1.31 \times 10^{-5} \text{ A}$$

$$I_B = I_E - I_C \approx 1.87 \times 10^{-8} \text{ A}.$$

- c) What are the base transport factor, α_T and the emitter injection efficiency, γ ? (15 points)

$$D_B = 6.5 \text{ cm}^2/\text{s}, \quad \tau_B = 1 \mu\text{s}, \quad L_B = \sqrt{D_B \tau_B} = \sqrt{6.5 \times 1 \times 10^{-6}} \approx 2.55 \times 10^{-3} \text{ cm}$$

$$\begin{aligned} \text{base transport factor } \alpha_T &= \frac{\partial I_{PE}(W_B)}{\partial I_{n(0)}} \approx 1 - \frac{W_B^2}{2L_B^2} \\ &= 1 - \frac{(266.6 \times 10^{-7} \text{ cm})^2}{2 \times (2.55 \times 10^{-3} \text{ cm})^2} \\ &\approx 0.999945 \end{aligned}$$

$$\begin{aligned} \text{emitter injection efficiency } \gamma &= \frac{\partial I_{PE}}{\partial I_E} \\ &\approx \frac{1}{1 + \frac{D_E W_B N_{AB}}{D_B W_E N_{DE}}} \\ &= \frac{1}{1 + \frac{2.6 \times 266.6 \times 1 \times 10^{18}}{6.5 \times 150 \times 5 \times 10^{20}}} \\ &\approx 0.9986 \end{aligned}$$

- d) What are the common base current gain, α_o and the common emitter current gain, β_o ? (10 points)

$$\text{Common base current gain } \alpha_o = \alpha_T \cdot Y \cdot M$$

$$\approx \alpha_T \cdot Y$$

$$= 0.999945 \times 0.9986$$

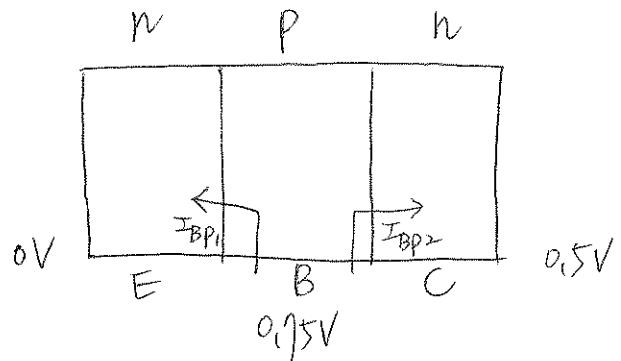
$$\approx 0.9985$$

$$\text{Common emitter current gain } \beta_o = \frac{\alpha_o}{1 - \alpha_o}$$

$$= \frac{0.9985}{1 - 0.9985}$$

$$\approx 665.7$$

(e) (Bonus question) if V_{CE} is 0.5V, that is Base-Collector junction is forward biased at 0.25V, what are I_C , I_E , and I_B ? Discussed. (20 points)

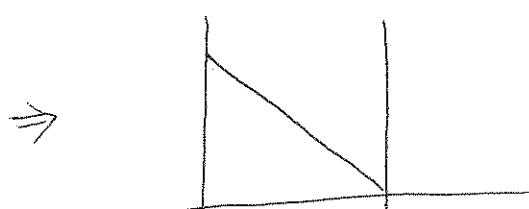


since the BE junction is the same as the Q.I. (a)
 \Rightarrow forward bias at 0.75V

and I_E is controlled by V_{BE}

$\therefore I_E$ is still the same as before (equation is the same)

At BC junction, minority carriers at base side ~~is~~ is $\propto \frac{n_i^2}{N_B} \exp\left(\frac{qV_{BC}}{kT}\right)$, which is relatively small compare to the minority carriers at BE junction base side
 \Rightarrow So we can still assume it's a straight line



So ~~is~~ $I_B = I_{BP1} + I_{BP2}$ as before

then $I_C = I_E - I_B$

2 (a) For the transistor in (1) if we want to reduce the neutral base width by 25% while maintaining the same current gain, β_0 , what is the new base doping concentration, assuming the same minority carrier (i.e. electron) mobility? (15 points)

$$W_{B,\text{neutral}} = 0.3 \mu\text{m} - \sqrt{\frac{26_i (\gamma_{B,\text{EE}} - 0.75)}{q \left(\frac{N_B N_E}{N_B + N_E} \right)}} \cdot \frac{N_E}{N_B + N_E} - \sqrt{\frac{26_i (\gamma_{B,\text{EC}} + 0.5)}{q \left(\frac{N_B N_C}{N_B + N_C} \right)}} \cdot \frac{N_C}{N_B + N_C}$$

$$\text{New } W_{B,\text{neutral}} = 0.267 \mu\text{m} \times 0.75 = 0.200 \mu\text{m}$$

By trial and error, $N_B, \text{new} = \underline{1.85 \cdot 10^{17} \text{ cm}^{-3}}$ gives $W_{B,\text{neutral}} = 0.2 \mu\text{m}$

~~WE~~

WE can be adjusted to retain the same β_0 .

Note that another solution exists if the metallurgical base width can be changed instead of WE.

two perspectives:

$$\text{new } W_B = W_{B,\text{old}} \times 75\%$$

(calculate N_B from W_B , adjust WE to retain the same β_0)

β_0 remains constant \rightarrow calculate N_B , adjust W_B to give required W_B for the new N_B .

(b) Do the same as in (a) if the minority carrier (i.e. electron) mobility is

$$\propto \frac{1}{1 + \left(\frac{N_A}{1 \times 10^{17} \text{ cm}^{-3}} \right)^{-0.25}} ? \quad (10 \text{ points})$$

For $W_{B,\text{new}} = 0.75 \times W_{B,\text{old}}$, trial and error gives $N_{B,\text{new}} = 1.85 \times 10^{17} \text{ cm}^{-3}$.

Note that another solution exists if the metallurgical base width can be changed instead of W_B .

(c) List two advantages and 2 disadvantages of this transistor (2b)
compared to that in (1) (10 points)

Transistor in 2b has smaller W_B , smaller N_A :

→ smaller base transition time, faster transistor ✓

→ Less electric field in junctions, less avalanche multiplication ✓

→ Smaller early voltage X

→ Larger base resistance X

(3) (a) The maximum voltage gain a BJT is capable of is given by $g_m r_{out}$ (EE151A). Show that $g_m r_{out}$ is to first order given by

$$g_m r_{out} = \frac{V_A}{V_T}$$

where V_A is the early voltage and V_T is the thermal voltage, kT/q . (8 points)

$$g_m = \frac{\partial I_C}{\partial V_{BE}} = \frac{I_C}{\frac{kT}{q}}$$

$$r_{out} = \frac{V_A}{I_C}$$

$$\Rightarrow g_m r_{out} = \frac{V_A}{\frac{kT}{q}} = \frac{V_A}{V_T} \quad \#$$

(b) What is the maximum voltage gain of the transistor in (1) (12 points)

$$V_A = \frac{q N_B W_B^2}{C_S}$$

$$g_m r_{out} = \frac{V_A}{V_T}$$

$$V_A = \frac{q W_B N_{AB}}{C_{DBC}}, \quad W_B = 266.6 \text{ nm}, \quad N_{AB} = 1 \times 10^{18} / \text{cm}^3, \quad x_{p2} = 11.5 \text{ nm}$$

$$x_{n2} = \frac{x_{p2} \cdot N_{AB}}{N_{DC}} = \frac{11.5 \times 1 \times 10^{18}}{8 \times 10^{16}} \approx 143.75 \text{ nm}$$

$$\begin{aligned} C_{DBC} &= \frac{C_S}{x_{p2} + x_{n2}} \\ &= \frac{11.7 \times 8.85 \times 10^{-14} \text{ F/cm}}{(11.5 + 143.75) \times 10^{-7} \text{ cm}} \\ &\approx 6.67 \times 10^{-8} \text{ F/cm}^2 \end{aligned}$$

$$\therefore V_A = \frac{1.6 \times 10^{-19} C \times 266.6 \times 10^{-7} \text{ cm} \times 1 \times 10^{18} / \text{cm}^3}{6.67 \times 10^{-8} \text{ F/cm}^2} \approx 63.95 \text{ V}$$

$$\therefore g_m r_{out} = \frac{V_A}{V_T} = \frac{63.95 \text{ V}}{0.026 \text{ V}} \approx 2460$$