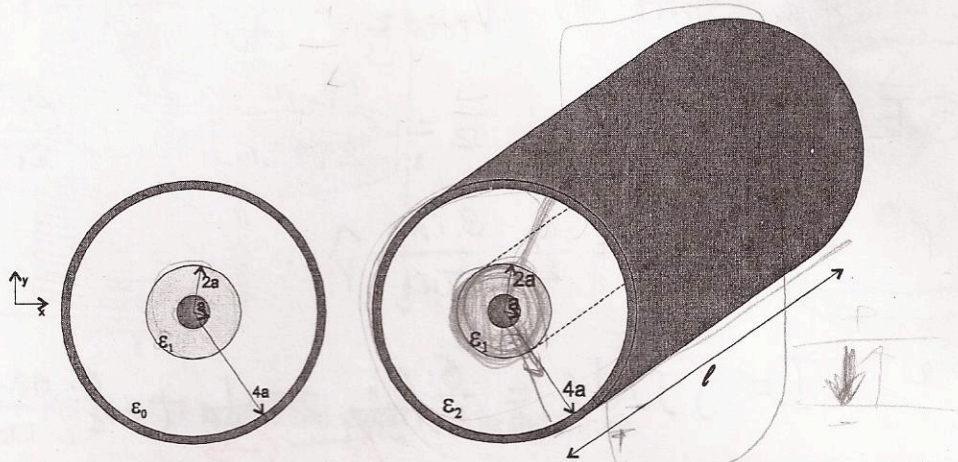


1. Coaxial capacitor (50 points)

Consider a piece of coaxial cable of length l with two dielectric layers with permittivities ϵ_1 and ϵ_2 . You may consider the inner conductor (radius a) and the outer conductor shell (radius $4a$) to be perfect conductors.



(a) What is the capacitance C between the inner and outer conductors? (Your answer should be in terms of only geometric and material parameters.)

$$C = \frac{Q}{V} = \frac{\int \epsilon \mathbf{E} \cdot d\mathbf{s}}{\int \mathbf{E} \cdot d\mathbf{l}}$$

$$\epsilon_1 \text{ for } r < 2a, \quad \epsilon_2 \text{ for } 2a < r < 4a$$

Using Gauss's Law,

$$\oint \mathbf{E} \cdot 2\pi r L = \frac{Q_{\text{in}}}{\epsilon}$$

$$\uparrow \mathbf{E} = \frac{Q_{\text{in}}}{\epsilon 2\pi r L}$$

$$= \frac{Q_{\text{in}}}{\epsilon 2\pi r L} \ln\left(\frac{2a}{a}\right) - a$$

$$\frac{\epsilon_1 \text{ for } r < 2a, \quad \epsilon_2 \text{ for } 2a < r < 4a}{\text{...}}$$

when $a < r < 2a$,

$$V = - \int \mathbf{E} \cdot d\mathbf{l} = - \int_a^{2a} \frac{Q_{\text{in}}}{\epsilon_1 2\pi r L} dr = - \frac{Q_{\text{in}}}{\epsilon_1 2\pi L} \ln(r) \Big|_a^{2a} = \frac{Q_{\text{in}}}{\epsilon_1 2\pi L} \ln\left(\frac{1}{2}\right)$$

when $2a < r < 4a$,

$$V = - \int \mathbf{E} \cdot d\mathbf{l} = - \int_{2a}^{4a} \frac{Q_{\text{in}}}{\epsilon_2 2\pi r L} dr = - \frac{Q_{\text{in}}}{\epsilon_2 2\pi L} \ln(r) \Big|_{2a}^{4a} = \frac{Q_{\text{in}}}{\epsilon_2 2\pi L} \ln\left(\frac{1}{2}\right)$$

$$\text{Thus } V_{\text{total}} = \frac{Q_{\text{in}}}{2\pi L} \ln\left(\frac{1}{2}\right) \left(\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2}\right) (V)$$

$\times -5$

$$C = \frac{Q}{V} = \frac{2\pi L}{\ln\left(\frac{1}{2}\right) \left(\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2}\right)} (F)$$

(b) Consider that the dielectric layers are lossy with conductivities σ_1 and σ_2 respectively. What is the resistance R between the inner and outer conductors?

Since Ohm's Law

$$R = \frac{V}{I} \quad \text{from part (a)} \quad V_{\text{total}} = \frac{Q_{\text{in}} \ln(\frac{1}{2})}{2\pi L} \left(\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2} \right) (V)$$

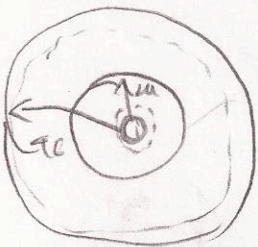
$$\vec{J} = \sigma \vec{E} \hat{r} \quad \text{at } r=a \quad \vec{E} = \frac{Q_{\text{in}}}{\epsilon_1 2\pi r L} \hat{r} \quad \vec{J}_1 = \frac{\sigma_1 Q_{\text{in}}}{\epsilon_1 2\pi r L} \hat{r}$$

$$\text{at } r=4a \quad \vec{J}_2 = \frac{\sigma_2 Q_{\text{in}}}{\epsilon_2 2\pi r L} \hat{r}$$

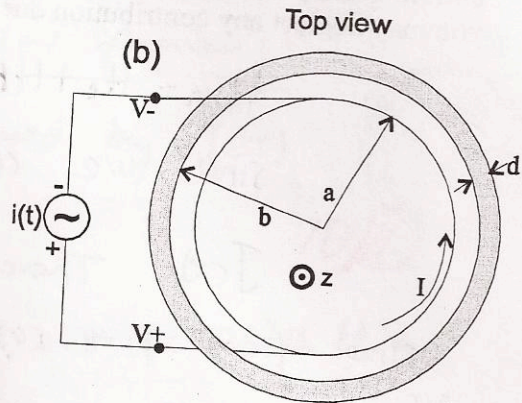
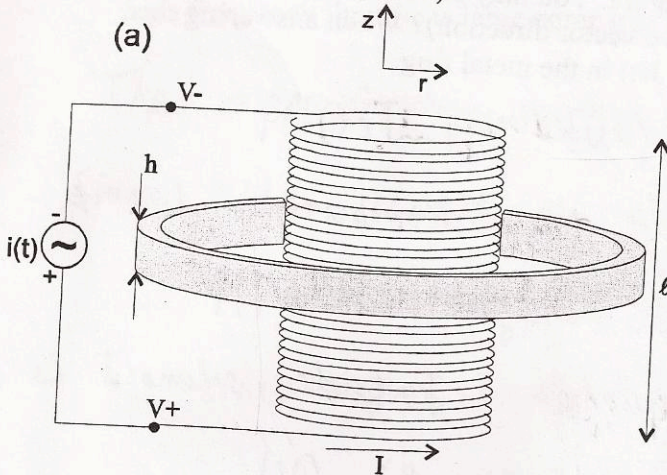
Therefore $I = \int \vec{J} \cdot d\vec{s} = \frac{\sigma_1 Q_{\text{in}}}{\epsilon_1} \frac{2\pi a L}{2\pi a L} + \frac{\sigma_2 Q_{\text{in}}}{\epsilon_2} \frac{2\pi 4a L}{2\pi 4a L}$
 $= Q_{\text{in}} \left(\frac{\sigma_1}{\epsilon_1} + \frac{\sigma_2}{\epsilon_2} \right) \quad (A)$

$$R = \frac{\ln(\frac{1}{2})}{2\pi L} \left(\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2} \right) \frac{Q_{\text{in}}}{\left(\frac{\sigma_1}{\epsilon_1} + \frac{\sigma_2}{\epsilon_2} \right)}$$

$$= \frac{\ln(\frac{1}{2}) (\epsilon_1 + \epsilon_2)}{2\pi L (\epsilon_2 \sigma_1 + \epsilon_1 \sigma_2)}$$



2. Inductor (50 points)



(a) (20 points) For part (a), ignore the metal ring in the figure.

Consider a solenoid with \$N\$ turns and length \$l\$, and radius \$a\$, is driven by a current source \$i(t) = i_0 \cos(\omega t)\$. As shown in the figure, we use the convention that a positive current is associated with current in the \$\phi\$ direction. You may assume that the solenoid is long (\$l \gg a\$). What is the voltage difference \$v(t) = V_+ - V_-\$ that appears across the terminals?

Your answer should be in terms of geometric, material, and fundamental parameters only (i.e. \$N, l, a, b, \epsilon, \mu, \sigma\$, etc.).

Since \$EMF = - \frac{d\Phi}{dt}\$, and \$i(t) = i_0 \cos(\omega t) = \text{Re} \{ \vec{I}_0 e^{j\omega t} \}\$.

and for long solenoid, \$\Lambda = N\Phi = N \int \vec{I}_0 = i_0 + 10\$

\$\Phi = \int \vec{B} \cdot d\vec{s} = \int \frac{\mu_0 \vec{I}(t) N}{l} ds = \frac{\mu_0 \vec{I} N \pi a^2}{l}\$ (assume \$B\$ outside solenoid \$\approx 0\$)

\$\therefore EMF = - \frac{d(\mu_0 \vec{I} N^2 \pi a^2)}{l dt} = - \frac{d\mu_0 N^2 \pi a^2}{l} \frac{d\vec{I}}{dt} = - \frac{\mu_0 N^2 \pi a^2}{l} \text{Re} \{ j\omega \vec{I}_0 e^{j\omega t} \}\$

\$= - \frac{\mu_0 N^2 \pi a^2}{l} \omega i_0 \sin(\omega t)\$ (v)

~~10~~

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(b) (20 points) A metal ring with height h , radius b , and thickness d , and conductivity σ is placed around the center of the solenoid as shown in the figure. You may assume $d \ll b$. What is the current density $\mathbf{J}(t)$ that flows in the metal ring (give vector direction)? When answering this, you may neglect any contribution due the currents $\mathbf{J}(t)$ in the metal ring.



$H_{in} = H_0 + H_1$ H_1 (caused by $\mathbf{J}(t)$)

since we can neglect the contribution due to $\mathbf{J}(t)$, therefore $H_{in} = H_0$.

since from part (a) we assume B outside solenoid is 0, we have EMF on ring = $\frac{\mu_0 N^2 I_0 a^2 \omega \sin(\omega t)}{L} \sin(\omega t)$. (V)

$R = \frac{L}{\sigma A} = \frac{2\pi b}{\sigma h d}$ and since $d \ll b$,

$\oint \mathbf{J}(t) \cdot d\mathbf{l} = \frac{\mu_0 N^2 I_0 a^2 \omega \sin(\omega t)}{2\pi b L} \sin(\omega t)$
 $= \frac{\mu_0 N^2 I_0 a^2 \omega \sin(\omega t)}{L 2\pi b} \sin(\omega t)$ (A)

$\oint \mathbf{J}(t) \cdot d\mathbf{l} = \int \mathbf{J}(t) \cdot d\mathbf{l} = \mathbf{J}(t) \cdot h d \oint$

$\mathbf{J}(t) = \frac{\mu_0 N^2 I_0 a^2 \omega \sin(\omega t)}{2\pi b L} \sin(\omega t) \hat{\phi}$ A/m²

$\int \mathbf{E} \cdot d\mathbf{l} = \frac{\mu_0 N^2 I_0 a^2 \omega \sin(\omega t)}{L 2\pi b} \sin(\omega t)$

$\mathcal{E} = \dots$

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- (c) (20 points) Does the approximation used in part (b) (neglecting any contribution due the currents $\mathbf{J}(t)$ in the metal ring) correspond to the low frequency limit (ω is small compared to τ_m^{-1}), or the high frequency limit (ω is large compared to τ_m^{-1})? Give a qualitative explanation why.

The approximation corresponds to low frequency ✓

Since $H_{in} = H_0 + H_1 \leftarrow H_1$ is caused by $\mathbf{J}(t)$.

$$\rightarrow H_1 = H_{in} - H_0 = \mathbf{E} \delta d. \Rightarrow$$

$$\text{since } \nabla \times \mathbf{E} = -\frac{d\mathbf{B}}{dt} = -\mu \frac{dH_{in}}{dt} \Rightarrow \int \mathbf{E} \cdot d\mathbf{l} = \omega r' \mu H_{in}$$

$$\Rightarrow \frac{dH_{in}}{dt} + \frac{H_{in}}{\tau_m} = \frac{H_0}{\tau_m} \quad \tau_m = \frac{\mu \delta d}{2}$$

And we assume $H_{in} = \vec{H}_{in} e^{j\omega t}$ $H_0 = \vec{H}_0 e^{j\omega t}$ plug in.

$$\text{we have } j\omega H_{in} e^{j\omega t} + \frac{H_{in} e^{j\omega t}}{\tau_m} = \frac{H_0 e^{j\omega t}}{\tau_m}$$

$$H_{in} e^{j\omega t} \left(j\omega + \frac{1}{\tau_m} \right) = \frac{H_0 e^{j\omega t}}{\tau_m}$$

$$\boxed{\frac{H_{in}}{H_0} = \frac{1}{1 + j\omega \tau_m}}$$

So when $\omega \rightarrow 0$, $\frac{H_{in}}{H_0} \approx 1$ corresponding to ✓

part(b) since the contribution of H_1 is negligible.

When $\omega \rightarrow \infty$, $\frac{H_{in}}{H_0} \ll 1$ This not correct approximation.